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Optimal adaptation to extreme rainfalls in current and future climate

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Abstract

More intense and frequent rainfalls have increased the number of urban flooding events in recent years, prompting adaptation efforts. Economic optimization is considered an efficient tool to decide on the design level for adaptation. The costs associated with a flooding to the T -year level and the annual capital and operational costs of adapting to this level are described with log-linear relations. The total flooding costs are developed as the expected annual damage of flooding above the T -year level plus the annual capital and operational costs for ensuring no flooding below the T -year level. The value of the return period T that corresponds to the minimum of the sum of these costs will then be the optimal adaptation level.

The change in climate, however, is expected to continue in the next century, which calls for expansion of the above model. The change can be expressed in terms of a climate factor (the ratio between the future and the current design level) which is assumed to increase in time. This implies increasing costs of flooding in the future for many places in the world. The optimal adaptation level is found for immediate as well as for delayed adaptation. In these cases the optimum is determined by considering the net present value of the incurred costs during a sufficiently long time span. Immediate as well as delayed adaptation is considered.

Key words: Urban flooding; rainfall impacts; extreme rainfalls; climate adaptation; economic optimization.

1. Introduction

Pluvial flooding of cities has become more frequent in recent years creating awareness of the needs for adaptation efforts. The increasing frequency of flooding has been attributed to climate change, and quite a few papers have assessed the expected development in urban rainfall extremes and the needs for adaptation efforts, e.g., Willems *et al.* (2012), Gregersen and Arnbjerg-Nielsen (2012), Arnbjerg-Nielsen *et al.* (2013) and Merz *et al.* (2014). Even without taking the changing climate into account it might be advantageous to revisit the urban drainage system in the light of current flooding risk. Urban drainage systems are generally designed by regulatory demands for safety return periods and thus not based on economic optimality.

Risk of flooding can be assessed in economic terms using the Expected Annual Damage (*EAD*) concept (e.g., Chow *et al.*, 1988). A method for analyzing the profitability of adaptation projects (e.g. Zhou *et al.*, 2012, 2013) is to carry out a series of cost-benefit calculations and comparing Net Present Values (*NPV*) of all encured costs and benefits. The *NPV* is the difference between the present value of benefits (reduction in damage costs) and the present value of construction and maintenance costs during the considered time period. While this can assure profitableness, it does not necessarily provide an optimal solution.

Fortunato *et al.* (2014) presented a procedure for obtaining the optimal design rainfall return period for urban drainage systems by minimizing the sum of *EAD* and the Equivalent Annual Costs (*EAC*) defined as the sum of annual capital and operational costs. The analysis, however, did not take climate development into account.

In the following the *EAD* concept will be thoroughly introduced, and then elaborated in the case of a log-linear relation between rainfall with return period T and the related damage $D(T)$ (e.g. Zhou *et al.*, 2012 and Olsen *et al.*, 2014). After adaptation, different modifications of the damage function will be considered. Then the optimal level of adaptation in current climate will be addressed assuming a log-linear relation between the return period T and the corresponding annual costs of adapting to this level. Contrary to Fortunato *et al.* (2014) the emphasis is laid on analytical solutions. However, by using numerical integration techniques results can be found as well, should the analytical requirements not be fulfilled.

In a changing climate *EAD* will increase during time in many places in the world, and therefore the Net Present Value (*NPV*) of all incurred costs during a sufficient long period should be minimized. After introducing a Climate Factor (*CF*) defined as the ratio between the design rain in a future changing climate and the design rain in the current climate the minimum *NPV* and the optimal adaptation level will be determined, while taking into account both immediate and delayed adaptation. Finally, the obtained results will be discussed and concluded.

2. Expected Annual Damage

If the T -year rainfall level is denoted x_T and the corresponding damage $D_x(x_T)$, the Expected Annual Damage (*EAD*) is obtained by the integral

$$EAD = \int_{x_{Ts}}^{\infty} D_x(x_T) f_x(x_T) dx_T = \int_{x_{Ts}}^{\infty} D_x(x_T) dF_x(x_T) \quad (1)$$

where $f_x(x_T)$ is the probability density function of the annual rainfall maximum, $F_x(x_T)$ is the cumulative distribution function, and x_{Ts} is the lowest level that implies damage costs. Here it is implicitly assumed that the T -year level refers to an annual maximum series, from which the T -year levels can be estimated. The exceedance probability of the T -year level is denoted $p = 1 - F_x(x_T)$. Thus we have $x_T = F^{-1}(1-p)$ and $dF_x(x_T) = -dp$, implying that

$$EAD = \int_0^{p_s} D_p(p) dp \quad (2)$$

where the argument in the damage function has been replaced such that $D_X(x_T) = D_p(p)$. This formulation is well-known (e.g., Chow *et al.*, 1988) and often utilized for calculation of EAD , although it is evident that it is difficult (impossible) to obtain values of the damage function for p close to 0.

In the following it is, however, more convenient to calculate EAD by integration over the return period, T . Using that $p = 1/T$ and $dp = -1/T^2 dT$, we get

$$EAD = \int_{T_s}^{\infty} \frac{D(T)}{T^2} dT \quad (3)$$

where the argument in the damage function again has been replaced such that now $D(T) = D_p(p)$. The integrand in Eq. (3) will be denoted risk density, *cf.* the notation probability density.

2.1 Log-linear damage function

It is now assumed that the damage function can be written as a log-linear relation, as observed by Zhou *et al.* (2012) and Olsen *et al.* (2014)

$$D(T) = a \ln T + b \quad \text{where} \quad D(T) = 0 \quad \text{for} \quad T = T_0 = \exp\left(-\frac{b}{a}\right) \quad (4)$$

For $T_0 \geq 1$ yr we get by integration of either Eq. (2) or Eq. (3)

$$EAD = a \exp\left(\frac{b}{a}\right) = \frac{a}{T_0} \quad (5)$$

assuming that damage will start where $D(T) = 0$. If damage starts at $T_s \geq T_0$, and $T_s \geq 1$ yr, we get

$$EAD = \frac{a}{T_s} \left(1 + \ln \frac{T_s}{T_0}\right) = a h(T_s) \quad (6)$$

whereby the function h has been introduced.

2.2 EAD after adaptation to the T -year level

After adaptation to the T -year level damage will now start at this level. EAD will then depend on the form of the damage curve after adaptation. We will consider four cases

- a damage curve shifted such that damage will start from 0 at the T -year level instead of at T_0 (or T_s)
- a shifted damage curve but with a changed slope

- the original damage curve being kept except that no damage will happen below the T -year level
- a gradual change from the shifted to the original damage curve depending on a form parameter γ , see Fig. 1.

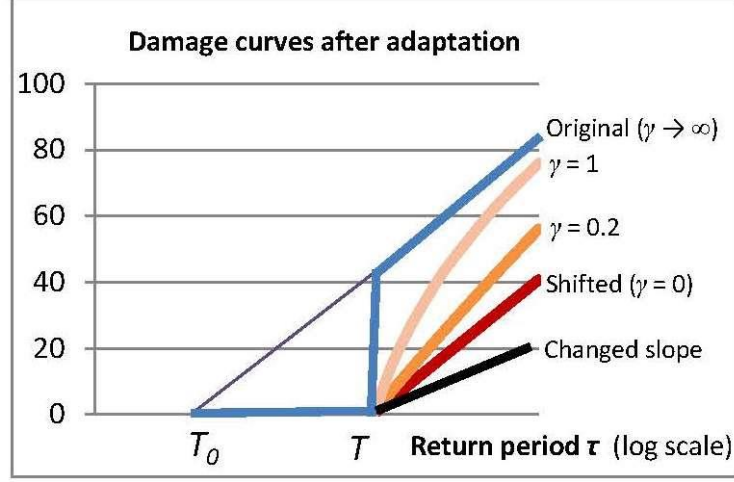


Fig. 1 Damage curves after adaptation to the T -year level.

Shifted damage curve

In this case we get

$$EAD(T) = \int_T^{\infty} \frac{D(\tau) - D(T)}{\tau^2} d\tau = \frac{a}{T} \quad (7)$$

Changed slope above T

Provided that a new slope of the damage curve ka is valid for all $T > T_s$, where a slope correction factor k has been introduced, we get

$$EAD(T) = \frac{ka}{T} \quad (8)$$

Original damage curve above T

Here we find

$$EAD(T) = \int_T^{\infty} \frac{D(\tau)}{\tau^2} d\tau = \frac{a}{T} \left(1 + \ln \frac{T}{T_0} \right) \quad (9)$$

Gradual change from 0 to the original damage curve

By introducing a form parameter γ ($0 \leq \gamma < \infty$), we get

$$EAD(T) = \int_T^{\infty} \frac{D(\tau) - D(T) \left(\frac{\tau}{T} \right)^{-\gamma}}{\tau^2} d\tau = \frac{a}{T} \left(1 + \left(1 - \frac{1}{1+\gamma} \right) \ln \frac{T}{T_0} \right) \quad (10)$$

where $\gamma = 0$ corresponds to the shifted damage curve, and $\gamma \rightarrow \infty$ corresponds to the original curve.

In general we have $EAD(T) = a g(T)$, where g can take on different forms depending on the actual conditions.

3. Optimal adaptation level in current climate

A plausible assumption may be that the equivalent annual costs EAC (capital and operational costs) corresponding to climate adaptation to the T -year level approximately follows a log-linear relation, as for example the data applied by Fortunato *et al.* (2014). Thus

$$EAC(T) = c \ln T + d \quad (11)$$

For the total annual costs TAC we get

$$TAC(T) = EAD(T) + EAC(T) \quad (12)$$

where EAD depends on the prevailing damage curve after adaptation. Obviously, the optimal adaptation level in an economic sense will be the one that minimizes TAC .

Shifted damage curve

By insertion of EAD from Eq. 7 we get

$$TAC(T) = \frac{a}{T} + c \ln T + d \quad (13)$$

Setting the derivative equal to 0 leads to

$$T_{opt} = \frac{a}{c} \quad (14)$$

Changed slope above T

Here we can just substitute a with the new slope using a correction factor k

$$T_{opt} = \frac{ka}{c} \quad (15)$$

Original damage curve above T

Using Eq. (9) TAC becomes

$$TAC(T) = \frac{a}{T} \left(1 + \ln \frac{T}{T_0} \right) + c \ln T + d \quad (16)$$

Setting the derivative equal to 0 leads to

$$T - \frac{a}{c} \ln \frac{T}{T_0} = 0 \quad (17)$$

from which T_{opt} can easily be found by iteration.

Gradually changed damage curve

For TAC we obtain using Eq. (10)

$$TAC(T) = \frac{a}{T} \left(1 + \left(1 - \frac{1}{1+\gamma} \right) \ln \frac{T}{T_0} \right) + c \ln T + d \quad (18)$$

Putting the derivative equal to 0 leads to

$$T - \frac{a}{c} \left[\left(1 - \frac{1}{1+\gamma} \right) \ln \frac{T}{T_0} + \frac{1}{1+\gamma} \right] = 0 \quad (19)$$

where T_{opt} again can be found by iteration.

4. Optimal adaptation in future climate

It can be approximately assumed that the climate factor CF (the ratio between future and current design rain) develops with time as a linear function (*e.g.* Park *et al.*, 2010). Thus

$$CF(t) \approx 1 + \theta t \quad \Rightarrow \quad \theta = \frac{CF(L) - 1}{L} \quad (20)$$

where L is the time horizon for the climate adaptation. Approximately the factor a in the log-linear damage relation will be proportional to the climate factor, see Appendix 1. Thus

$$a(t) = a CF(t) = a(1 + \theta t) \quad (21)$$

For EAD we have

$$EAD(t, T) = a(t) g(T) \quad (22)$$

where the function $g(T)$ depends on the actual damage curve. For immediate adaptation the Net Present Value (NPV) of all incurred costs assuming a discount rate r can then be expressed

$$NPV(T) = \sum_{t=1}^L (a(t)g(T) + EAC(T))(1+r)^{-t} \quad (23)$$

and the optimal return period level determined indirectly by finding

$$NPV(T_{opt}) = \min_T NPV(T) \quad (24)$$

Taking delayed adaptation into account, optimization can be carried out with respect to both T and t_* , where t_* is the adaptation time. The NPV becomes

$$NPV(t_*, T) = \sum_{t=1}^{t_*} a(t) h(T_s) (1+r)^{-t} + \sum_{t=t_*+1}^L (a(t)g(T) + EAC(T))(1+r)^{-t} \quad (25)$$

and

$$\min_{t_*, T} NPV(t_*, T) \quad (26)$$

will provide the optimal combination of adaptation time and adaptation level. For a fixed chosen adaptation time a conditionally optimal T can be found. In Appendix 2 closed form solutions for the Net Present Values and optimal T -values are developed assuming that the shifted damage function is valid.

In the general case the NPV is presented in closed form in Appendix 3 together with an equation from which the optimal T -value can be found by iteration. Prevailing values for adaptation time t_* , discount rate r , gradient in the climate factor θ , slope in the log-linear damage function a , return period for which the log-linear damage function is zero T_0 , return period where damage starts T_s , slope correction parameter in the damage function after adaptation k , form parameter in the damage function after adaptation γ and slope in the log-linear adaptation cost function c can be applied.

5. Example

The damage costs for the different levels of extreme rain in Table 1 have been adopted from Olsen *et al.* (2014). The data originate from the city of Odense in Denmark and may not be representative for other cities. They approximately follow a log-linear relation and are as such representative for a number of analyzed cases. T_* in the first row denotes return periods estimated in partial duration (or peak over threshold) series. In the second row T_* has for $T_* \leq 10$ yr been transformed to annual maximum series return periods using the formula (Rosbjerg, 1977)

$$T = \left[1 - \exp\left(-\frac{1}{T_*}\right) \right]^{-1} \quad (27)$$

Table 1 Damage costs as function of return periods for extreme rainfall (adopted from Olsen *et al.* (2014)).

T_*	(yr)	2	3	5	7	10	20	50	60	75	100	125	150	200	250	500	1000
T	(yr)	2,54	3,53	5,52	7,51	10,5	20	50	60	75	100	125	150	200	250	500	1000
$D(T)$	(10^6 DKK)	2	5	7	8	10	21	8	34	36	39	45	47	55	57	70	82

The plot in Fig. 2 confirms an approximate log-linear relation between return period and damage costs. The risk density is shown in Fig. 3.

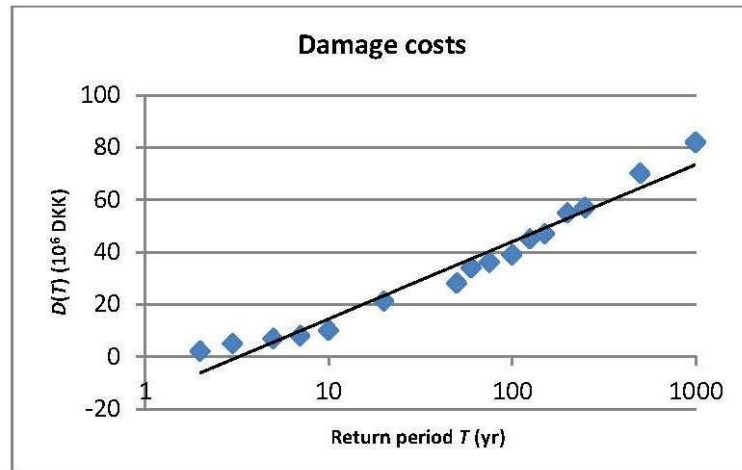


Fig. 2 Damage costs as function of the return period of extreme rainfalls.

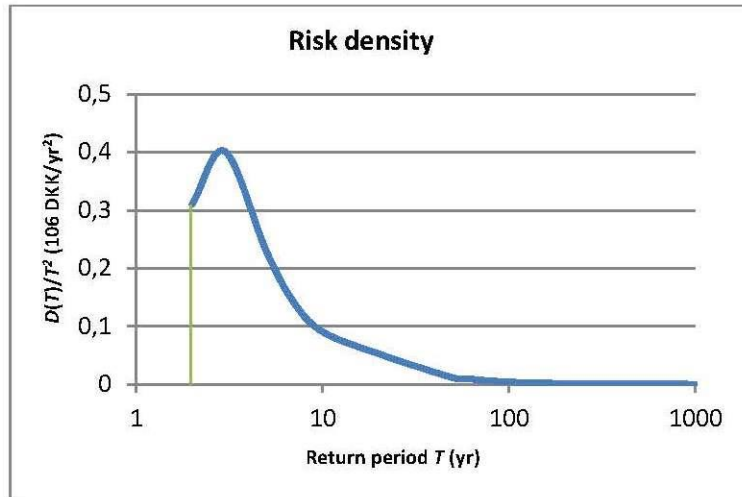


Fig. 3 Risk density as function of the return period of extreme rainfalls.

From Fig. 3 it is seen that the contribution from rare events to the *EAD* is minor.

To obtain the parameters for optimization we plot the damage curve using natural logarithms of T in Fig. 4.

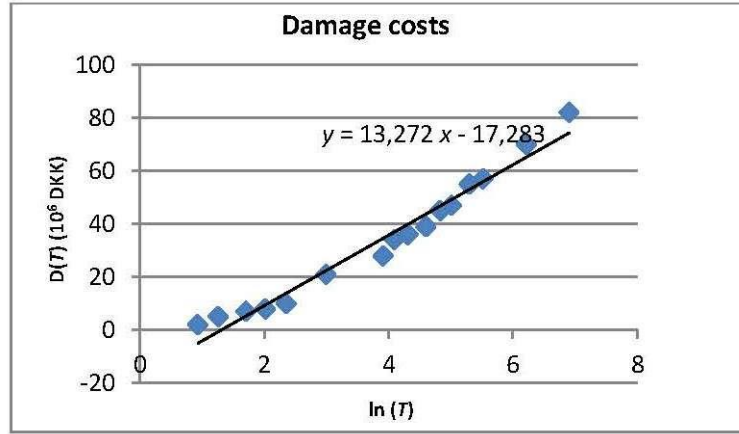


Fig 4. Damage costs as function of the natural logarithm of T .

It is seen that $a = 13.3 \cdot 10^6$ DDK/yr and $b = -17.3 \cdot 10^6$ DDK/yr. Thus from Eq. (4) $T_0 = 3.67$ yr $>$ 1 yr, and from Eq. (5) we get $EAD = 3.62 \cdot 10^6$ DDK/yr.

Estimation of the adaptation costs as function of the adaptation level has led to the values $c = 0.5 \cdot 10^6$ DDK/yr and $d = -0.65 \cdot 10^6$ DDK/yr in Eq. (11).

5.1 Adaptation in current climate

Assuming that the shifted damage curve is valid, we obtain from Eq. (14) that $T_{opt} = 26.6$ yr and from Eq. (13) that $TAC(T_{opt}) = 1.49 \cdot 10^6$ DDK/yr. These results are illustrated in Fig. 5.

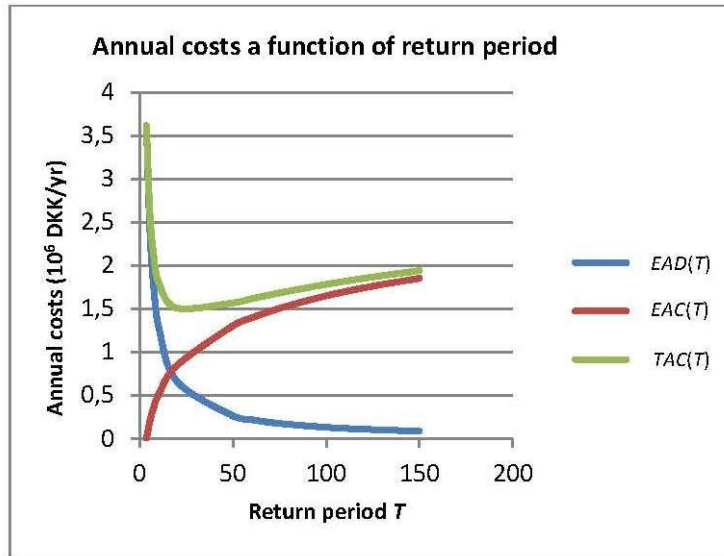


Fig. 5 Annual costs as function of the return period.

As can be noted from Fig. 5, it is much more expensive to underestimate than overestimate the optimal return period. This is also evident from the results of Fortunato *et al.* (2014).

An indication of the uncertainty in the obtained optimal return period can be obtained using a simple first order analysis leading to

$$CV_{T_{opt}} \approx \sqrt{CV_a^2 + CV_c^2} \quad (28)$$

Thus a 10% uncertainty in both a and c will lead to a 14% uncertainty in T_{opt} .

5.2 Adaptation in future climate

Let us assume that the shifted damage curve still is valid and that $L = 100$ yr and $r = 0.03$. Two different climate factors are considered, $CF(L) = 1.4$ and $CF(L) = 1.7$.

Immediate adaptation

By using Eqs. (23) or (A2.2) we can plot the net present value as function of the return period in Fig. 6.

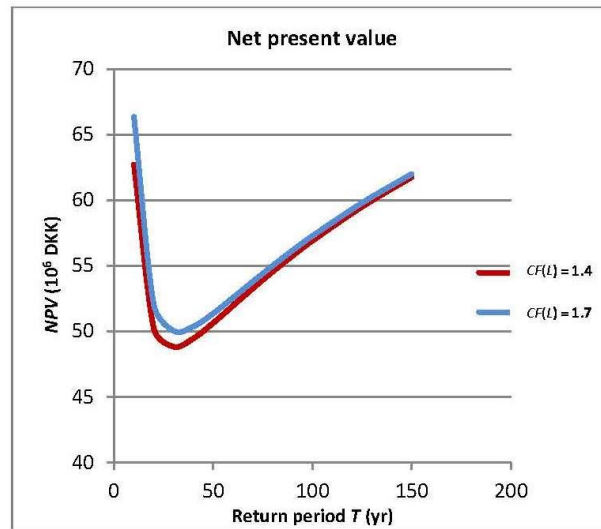


Fig. 6 Net present value of all incurred costs as function of the return period.

It is seen that the optimal return period has increased slightly. Using Eq. (A2.4) we get $T_{opt} = 29.6$ yr for $CF(L) = 1.4$ and $T_{opt} = 31.8$ yr for $CF(L) = 1.7$. Using Eq. (A2.2) the minimum net present value is found to $48.9 \cdot 10^6$ DDK/yr for $CF(L) = 1.4$ and $50.0 \cdot 10^6$ DDK/yr for $CF(L) = 1.7$.

It should be noticed that inclusion of climate development in the example sharpens the minimum such that due to the increasing damage costs with time the tendency for overestimation to be more expensive than underestimation becomes less pronounced.

Delayed adaptation

By use of Eqs. (25) or (A2.1) the effect of delayed adaptation can be analyzed. In the present case the optimal adaptation level T_{opt} is moderately increased, see Fig. A2.1. Growth in the NPV minimum with delay time, however, is pronounced, see Fig. 7. This is primarily attributed to the

expected flooding costs encountered before the adaptation has taken place. Both figures also show the relative effects of the different climate factors.

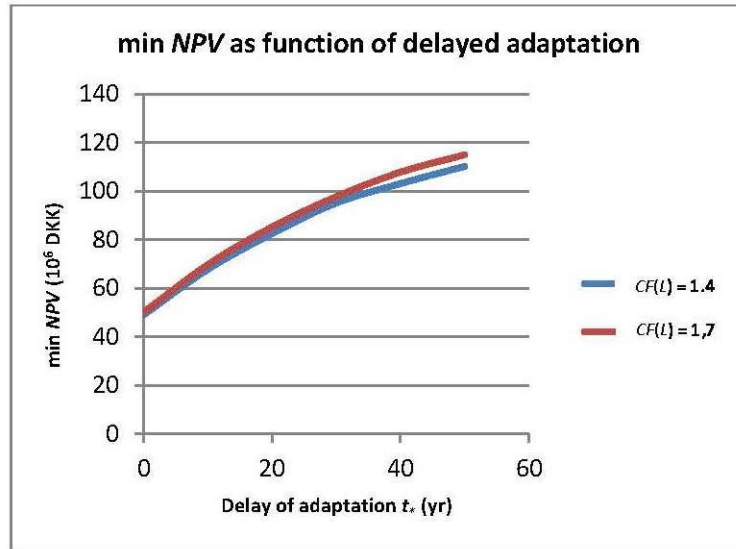


Fig. 7 Minimum of *NPV* as function of delayed adaptation.

6. Discussion

The optimization has been presented using log-linear relations for both the damage costs caused by extreme rainfall with a given return period and for the costs of adaptation to such rainfalls, which provides analytical advantages. Although these relations appear plausible, they may not always be fulfilled. Therefore, it should be emphasized that the developed optimization procedure can also be carried out with arbitrary cost functions using numerical integration.

Uncertainty is inherent in the economic calculations. Cost functions are often crude estimates, and parameters like the discount rate can always be discussed. Another contribution to uncertainty is the linkage between the return period and the extreme rainfall magnitude. This is outside the scope of the present paper, but has been thoroughly treated by Arnell (1989). Altogether these different sources of uncertainty make it advisable to carry out a sensitivity analysis before a final decision is taken.

7. Conclusions

A procedure for estimating the optimal adaptation level in economic terms has been developed and exemplified using log-linear functions for the damage caused by extreme rainfalls and the costs of adapting to these rainfalls. Solutions corresponding to different options for how the damage cost function may change after adaptation have been considered, and corresponding expressions for the expected annual damage after adaptation have been developed. Optimal adaptation levels in

economic terms have been determined in the cases of both immediate and delayed adaptation. For immediate adaptation the total annual costs have been minimized, while for delayed adaptation the net present value was minimized. The results indicate that the optimal adaptation level is relatively stable, if a shifted damage curve is valid, but delaying the adaptation raises the costs notably, primarily due to expected damage costs until the adaptation is carried out. Due to the uncertainty involved in economic optimization the found optimum should not be considered the final answer, but rather a starting point for more refined design efforts.

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Appendix 1: Relation between climate factor and slope of damage function

Consider the situation at the end of the planning period, say after L years. The design rain without climate change is denoted x_L and with accountancy of climate change ξ_L . Thus

$$\xi_L = CF(L) x_L \quad (A1.1)$$

The corresponding return periods are

$$T_{\xi_L} = \frac{1}{1 - F_X(\xi_L)} \quad \text{and} \quad T_{x_L} = \frac{1}{1 - F_X(x_L)} \quad (A1.2)$$

It is anticipated that the cost of exceeding x_L in L years' time will equal the cost of exceeding ξ_L today

$$a(L) \ln T_{x_L} + b = a \ln T_{\xi_L} + b \quad (A1.3)$$

This implies that

$$a(L) = a \frac{\ln \frac{1}{1 - F_X(\xi_L)}}{\ln \frac{1}{1 - F_X(x_L)}} = a \frac{\ln(1 - F_X(\xi_L))}{\ln(1 - F_X(x_L))} \quad (A1.4)$$

Now assume that F_X approximately has exponential tail behavior, that is $F_X(x) \approx 1 - \exp(-\lambda x)$. Then

$$a(L) \approx a \frac{\xi_L}{x_L} = a \text{ CF}(L) \quad (\text{A1.5})$$

Appendix 2: NPV and T_{opt} assuming a shifted damage function

In the case of a shifted damage function and $T_s = T_0$ the continuous counterpart to Eq. (25) can be written

$$\begin{aligned} NPV(t_*, T) &= \int_0^{t_*} EAD(t, T_0) e^{-rt} dt + \int_{t_*}^L (EAD(t, T) + EAC(t, T)) e^{-rt} dt \\ &= \frac{a}{T_0} \int_0^{t_*} e^{-rt} dt + \frac{a\theta}{T_0} \int_0^{t_*} t e^{-rt} dt + \frac{a}{T} \int_{t_*}^L e^{-rt} dt + \frac{a\theta}{T} \int_{t_*}^L t e^{-rt} dt + (c \ln T + d) \int_{t_*}^L e^{-rt} dt \\ &= \left(\frac{a}{rT_0} + \frac{a\theta}{r^2 T_0} \right) (1 - e^{-rt_*}) - \frac{a\theta}{rT_0} t_* e^{-rt_*} + \left(\frac{a}{rT} + \frac{a\theta}{r^2 T} \right) (e^{-rt_*} - e^{-rL}) \\ &\quad + \frac{a\theta}{rT} (t_* e^{-rt_*} - L e^{-rL}) + \left(\frac{c}{r} \ln T + \frac{d}{r} \right) (e^{-rt_*} - e^{-rL}) \end{aligned} \quad (\text{A2.1})$$

In the special case of $t_* = 0$, i.e. immediate adaptation, we get

$$NPV(T) = \left(\frac{a}{rT} + \frac{a\theta}{r^2 T} + \frac{c}{r} \ln T + \frac{d}{r} \right) (1 - e^{-rL}) - \frac{a\theta L}{rT} e^{-rL} \quad (\text{A2.2})$$

Setting the derivative of Eq. (A2.1) with respect to T equal to 0 and solving for T result in

$$T_{opt}(t_*) = \frac{\left(1 + \frac{\theta}{r} \right) (e^{-rt_*} - e^{-rL}) + \theta (t_* e^{-rt_*} - L e^{-rL})}{\frac{c}{a} (e^{-rt_*} - e^{-rL})} \quad (\text{A2.3})$$

which in the special case of $t_* = 0$ gives the optimal T -year level for immediate adaptation

$$T_{opt} = \frac{\left(1 + \frac{\theta}{r} \right) (1 - e^{-rL}) - \theta L e^{-rL}}{\frac{c}{a} (1 - e^{-rL})} \quad (\text{A2.4})$$

Eq. (A2.3) is illustrated in Fig. A2.1 with use of the same parameters as introduced in the example.

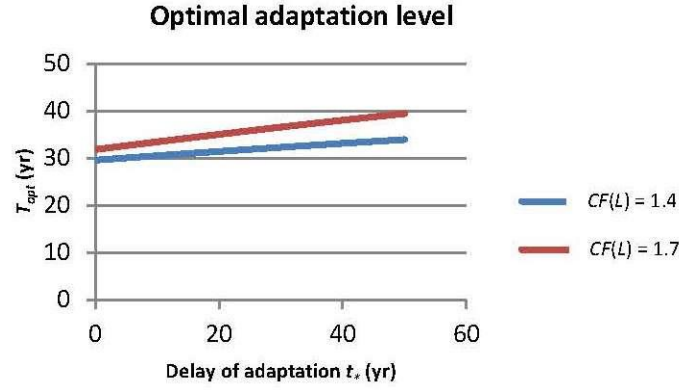


Fig. A2.1 Optimal adaptation level as function of adaptation delay.

It can be seen that a delay will moderately increase the optimal return period.

Appendix 3: NPV and T_{opt} in the general case

In the general case the net present value becomes

$$\begin{aligned}
 NPV(t_*, T) = & \left(\frac{a}{rT_0} + \frac{a\theta}{r^2T_0} + \frac{a}{T_s} \ln \frac{T_s}{T_0} + \frac{a\theta}{r^2T_s} \ln \frac{T_s}{T_0} \right) (1 - e^{-rt_*}) - \left(\frac{a\theta}{rT_0} + \frac{a\theta}{rT_s} \ln \frac{T_s}{T_0} \right) t_* e^{-rt_*} \\
 & + \left(\frac{a}{rT} + \frac{a\theta}{r^2T} \right) (e^{-rt_*} - e^{-rL}) \\
 & + \frac{ka}{rT} \left[1 + \left(1 - \frac{1}{1+\gamma} \right) \ln \frac{T}{T_0} \right] \left[\left(1 + \frac{\theta}{r} \right) (e^{-rt_*} - e^{-rL}) + \theta (t_* e^{-rt_*} - L e^{-rL}) \right] \\
 & + \left(\frac{c}{r} \ln T + \frac{d}{r} \right) (e^{-rt_*} - e^{-rL})
 \end{aligned} \tag{A3.1}$$

and the optimal return period must be found by iteration in the expression

$$T - \frac{\left(\frac{1}{1+\gamma} + \left(1 - \frac{1}{1+\gamma} \right) \ln \frac{T}{T_0} \right) \left[\left(1 + \frac{\theta}{r} \right) (e^{-rt_*} - e^{-rL}) + \theta (t_* e^{-rt_*} - L e^{-rL}) \right]}{\frac{c}{ka} (e^{-rt_*} - e^{-rL})} = 0 \tag{A3.2}$$